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Removal of the superficial zone of bovine articular cartilage does not increase its frictional coefficient

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Summary

Objective: To investigate the role of the superficial zone in regulating the frictional response of articular cartilage. This zone contains the superficial protein (SZP), a proteoglycan synthesized exclusively by superficial zone chondrocytes and implicated in reducing the friction coefficient of cartilage.

Design: Unconfined compression creep tests with sliding of cartilage against glass in saline were carried out on fresh bovine cylindrical plugs (26 mm, $n = 35$) obtained from 16 bovine shoulder joints (ages 1–3 months). In the first two experiments, friction tests were carried out before and after removal of the superficial zone ($\sim 100 \mu\text{m}$), in a control and treatment group, using two different applied load magnitudes (4.4 N and 22.2 N). In the third experiment, friction tests were conducted on intact surfaces and the corresponding microtomed deep zone of the same specimen.

Results: In all tests the friction coefficient exhibited a transient response, increasing from a minimum value (μ_{\min}) to a near-equilibrium final value (μ_{eq}). No statistical change ($P > 0.5$) was found in μ_{\min} before and after removal of the superficial zone in both experiments 1 and 2. However, μ_{eq} was observed to decrease significantly ($P < 0.001$) after removal of the surface zone. Results from the third experiment confirm that μ_{eq} is even lower at the deep zone. Surface roughness measurements with atomic force microscopy (AFM) revealed an increase in surface roughness after microtoming. Immunohistochemical staining confirmed the presence of SZP in intact specimens and its removal in microtomed specimens.

Conclusions: The topmost ($\sim 100 \mu\text{m}$) superficial zone of articular cartilage does not have special properties which enhances its frictional response.

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Key words: Cartilage, Friction, Interstitial fluid pressurization, Superficial zone protein, Atomic force microscopy.

Introduction

The primary function of articular cartilage is to provide low friction and wear at contacting joint surfaces. Several mechanisms have been proposed to explain the remarkable frictional characteristics of cartilage^{1–10}. One of these proposed mechanisms is premised on the special tribological properties of a mucinous glycoprotein present in synovial fluid, lubricin, described by Swann, Radin and co-workers^{4,5}. Recent studies have established a homology of lubricin with superficial zone protein (SZP)^{11,12}, a proteoglycan synthesized exclusively by superficial zone chondrocytes^{13–15}. It has been inferred, but not directly verified, that the presence of SZP in the superficial zone of cartilage should impart beneficial tribological properties to contacting articular layers.

This study investigated the potential special role of the superficial zone in regulating the frictional response of articular cartilage, by measuring the friction coefficient of bovine articular cartilage against glass, before and after removal of the topmost superficial tangential zone, where SZP is localized. The hypothesis was that the friction coefficient of articular cartilage would increase after

microtoming of the superficial zone. Additional control groups were tested to help minimize confounding effects in the interpretation of results. Atomic force microscopy (AFM) measurements were also performed to characterize the surface topography before and after microtoming.

Materials and methods

Three friction experiments were conducted in this study. In the first two experiments, cartilage samples were divided into a control group and a treatment group. The friction coefficient was measured twice in each sample: in the treatment group, the first friction test on the sample was performed with the superficial tangential zone intact and the second test was performed after microtoming to remove the superficial zone. In the control group, both tests were performed with the surface intact. The second experiment was similar to the first, but employed a higher applied load in the friction test to investigate whether results might be dependent on load magnitude. In the third experiment, one group of samples was used; two friction tests were performed on each sample, one on the intact articular surface and the other on the microtomed deep zone.

SPECIMEN PREPARATION

Fresh bovine shoulder joints were obtained from a local abattoir (19 joints, ages 1–4 months). Joints were stored at

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4°C, with an intact capsule, for no more than 4 days prior to dissection. Following joint dissection, full thickness osteochondral plugs (Ø6 mm) were harvested from the humeral head. Underlying bone and vascularized tissue (~400 µm thick) were removed from the deep zone of the cartilage plugs using a sledge microtome (model 1400; Leitz, Rockleigh, NJ), leaving the articular surface intact. A total of 58 cylindrical cartilage samples were obtained. Twelve samples were used in each of the first two experiments and 13 in the third experiment. Nine samples were used for immunohistochemical staining for SZP and 12 were used for AFM measurements of surface topography.

FRICITION MEASUREMENTS

The friction coefficient between cartilage and glass was measured in phosphate buffered saline (PBS), under the configuration of unconfined compression creep (Fig. 1), with intermittent sliding over logarithmic time increments (sliding velocity = 1 mm/s). Reciprocal sliding motion was provided by a computer controlled translation stage (Model

PM500-1L, Newport Corporation, CA). The range of translation for the sliding stage was ± 1.5 mm in the first experiment (where the normal applied load was 4.4 N) and ± 4.5 mm in the second and third experiments (normal load of 22.2 N). The greater range of translation in the second and third experiments was prescribed to better overcome the shear deformation of the sample and ensure relative sliding between the surfaces. The normal load was applied using a voicecoil load actuator (model LA17-28-000A, BEI Kimco Magnetics Division, San Marcos, CA), ramped up from zero to its prescribed value over a period of 10 s, then maintained constant over the remaining duration of the test. Normal and frictional loads were measured with a multi axial load cell mounted on the translation stage (Model 20E12A-M25B, JR3 Inc., Woodland, CA). The friction force and normal force were averaged over the back and forth portions of each cycle of reciprocal motion and the friction coefficient was obtained from the ratio of these values. When plotting the friction coefficient, the values at consecutive logarithmic increments were connected with a straight line, producing continuous curves as a function of time. Cartilage creep displacement was monitored with a linear variable differential transformer (model PR 812, Macro Sensors, Pennsauken, NJ). All tests were terminated after 2500 s. The normal force, frictional force and creep displacement were monitored throughout the test with data acquisition hardware and software (model PCI-6030E & Labview v6.1; National Instruments, Austin, TX). The time-dependent friction coefficient, μ_{eff} , was calculated from the ratio of the friction force to the normal force. The minimum value of μ_{eff} was denoted by μ_{min} and the final near-equilibrium value, achieved at 2500 s, was denoted by μ_{eq} . Between tests, the glass platen was thoroughly cleaned with distilled water, alcohol and scrubbing.

EXPERIMENTS

In the first two experiments, samples were equally divided into the control and treatment groups; averages and standard deviations of specimen thickness (h) in each group are reported in Table I. Two friction tests were performed on each sample. In the first test, the articular surface was left intact in both control and treatment groups. At the completion of the test, the sample was equilibrated in PBS for 2 h to recover from creep deformation. In the treatment group, the sample was then frozen in an embedding matrix on the freezing stage of a sledge microtome (~10 min), and ~80–180 µm of the superficial tangential zone was removed (Table I). Control group specimens were similarly embedded on the freezing stage but were not microtomed.

In the third experiment, frictional tests were performed on the articular surface and the corresponding microtomed deep zone of each sample. A 2 h recovery period was similarly used between tests. The order of testing of surfaces was randomized.

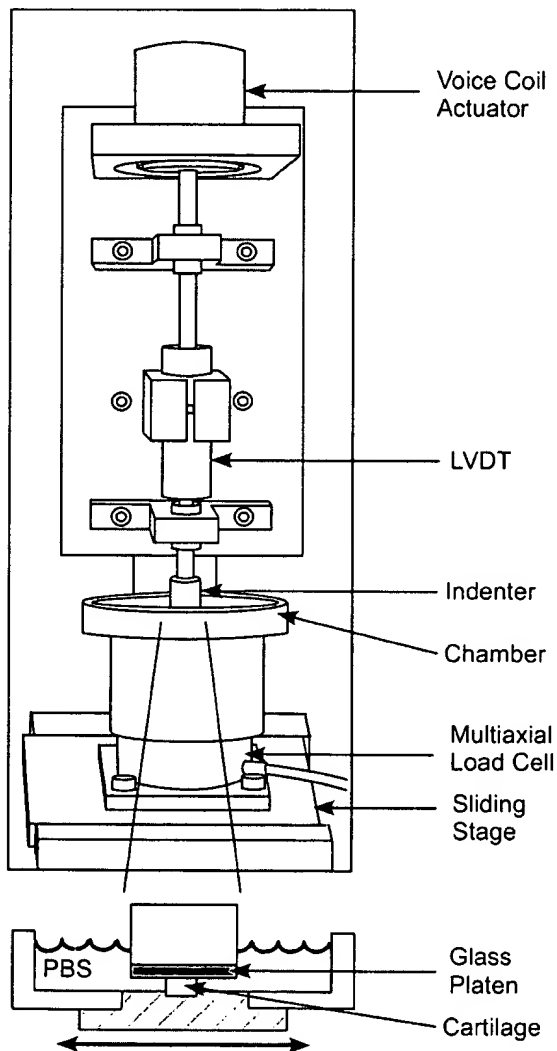


Fig. 1. Schematic of friction device.

Table I
Summary of cartilage sample thicknesses in experiments 1 and 2

h (mm)	Experiment 1 (4.4 N)		Experiment 2 (22.2 N)	
	Control	Treated	Control	Treated
Test 1	1.85 ± 0.17	1.80 ± 0.22	2.15 ± 0.40	2.04 ± 0.45
Test 2	1.85 ± 0.17	1.62 ± 0.23	2.15 ± 0.40	1.96 ± 0.44

IMMUNOHISTOCHEMICAL STAINING FOR SZP

Samples were divided into three groups: (1) Osteochondral plugs with intact superficial tangential zone ($n = 3$); (2) chondral plugs with intact superficial tangential zone and microtomed deep zone ($n = 3$); and (3) chondral plugs microtomed both at the superficial tangential zone and at the deep zone ($n = 3$). Samples were fixed overnight at 4°C in acid formalin ethanol (70% ethanol, 3.7% formaldehyde, 5% acetic acid). Fixed samples were dehydrated with a graded series of ethanol, embedded in paraffin blocks (Tissue Prep, Fisher Scientific, Fair Lawn, NJ), sectioned on a rotary microtome (model 2030, Leica, Bannockburn, IL) into 10 μm thick sections, and affixed onto glass slides. Prior to staining, specimens were deparaffinized with Citrosolv (Fisher Scientific, Fair Lawn, NJ) and rehydrated. Immunohistochemical analysis was carried out with a polyclonal antibody directed against SZP (06A10, kindly provided by Dr Carl Flannery, Wyeth Research Division, Cambridge, MA). Sections were washed in PBS and blocked with 10% normal goat serum (NGS, in PBS) for 10 min at room temperature, followed by incubation with primary antibody (16 $\mu\text{g}/\text{ml}$ in 10% NGS) for 12 h at 4°C. Sections were then washed with PBS, and incubated with Alexa Fluor 488 conjugated goat anti-rabbit secondary antibody (Molecular Probes, Eugene, OR) at 20 $\mu\text{g}/\text{ml}$ in 10% NGS for 1 h at room temperature. After extensive washing with dH_2O , samples were then treated with Propidium Iodide Nucleic Acid Stain (Molecular Probes, Eugene, OR) at 10 $\mu\text{g}/\text{ml}$ for 5 min to visualize nuclei, washed three times with dH_2O , and cover-slipped with Gel/Mount (Biomedica, Foster City, CA). On each slide, one section was maintained as a non-immune control, following the procedure described above with 10% NGS substituted for primary antibody. Sections were viewed using an inverted microscope (model IX-70, Olympus, Melville, NY) equipped with a confocal imaging system with dual wavelength excitation at 488 and 568 nm and imaged at 20 \times and 50 \times magnification using a 20 \times objective with digital magnification. All images were acquired using the Fluoview control software (Olympus, Japan).

IMAGING WITH ATOMIC FORCE MICROSCOPY

Samples, which were stored at 4°C for no more than 24 h before imaging, were divided into three groups: (1) intact articular surface ($n = 4$); (2) microtomed superficial zone ($n = 4$); (3) microtomed deep zone ($n = 4$). Each sample was affixed to a polystyrene disk with cyanoacrylate adhesive, and imaged in PBS, at 2–4 locations on the surface of interest (Bioscope AFM, Digital Instruments, Santa Barbara, CA), following our recently described protocol¹⁶. A scan size of 100 \times 100 \times 12 μm was obtained in contact mode, with an image size of 256 \times 256 pixels using an unsharpened silicon-nitride microlever probe (Veeco Instruments, Santa Barbara, CA). Average surface roughness was determined using a centerline average (R_a) measured using Nanoscope software (Digital Instruments, Santa Barbara, CA). R_a was determined for the entire 100 \times 100 μm image.

STATISTICAL ANALYSES

In experiments 1 and 2, three-way analysis of variance (ANOVA) was used to analyze differences in μ_{\min} and μ_{eq} between control and treatment groups, between the first and second friction test (repeated measure), and between

the different loading magnitudes (experiment 1 and experiment 2). When significant differences were detected, Bonferroni-corrected *post-hoc* testing of the means was performed. In experiment 3, one-way ANOVA was

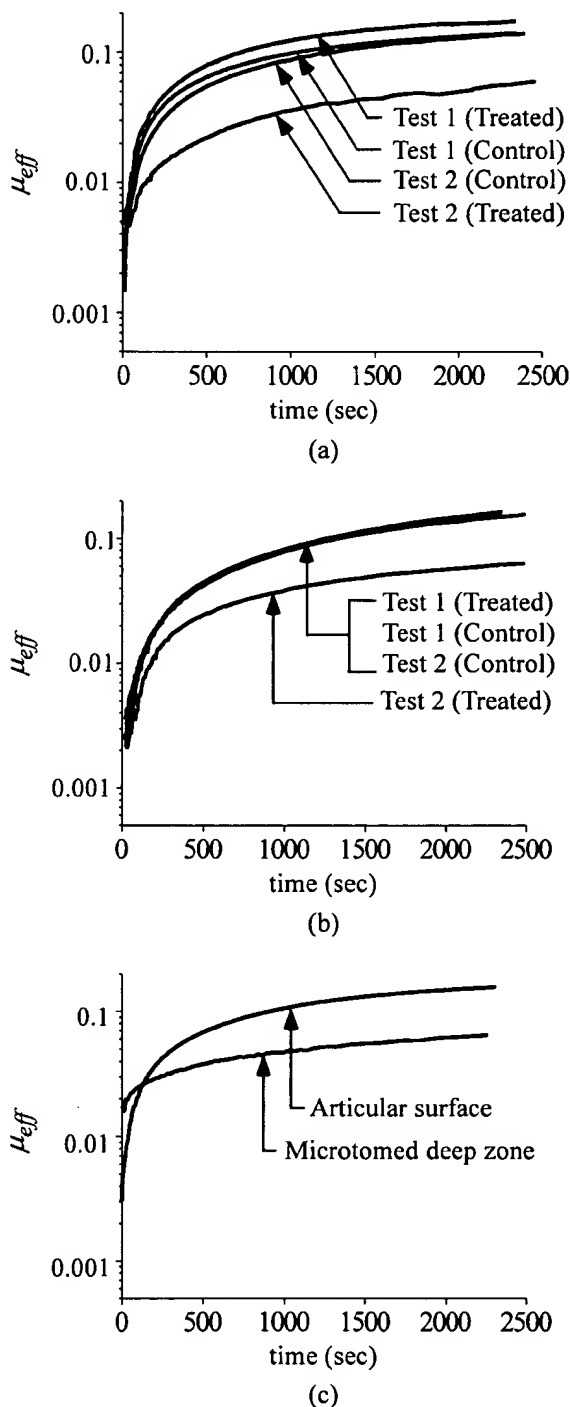


Fig. 2. Average curves showing variation of the effective friction coefficient (μ_{eff}) as a function of time for (a) test 1 and test 2 in control and treated groups from experiment 1; (b) test 1 and test 2 in control and treated groups from experiment 2; (c) friction tests on articular surface and corresponding side opposite the surface (microtomed deep zone) from experiment 3.

performed to detect differences in μ_{\min} and μ_{eq} between the articular surface and the deep zone. For surface roughness measurements, R_a at the intact or microtomed articular surface and (when applicable) at the microtomed deep zone was compared among the three tested groups using one-way ANOVA ($n = 12$ for group 1, $n = 11$ for group 2 and $n = 11$ for group 3). For all analyses, statistical significance was accepted for $P \leq 0.05$, with $\alpha = 0.05$.

Results

In all tests, the friction coefficient μ_{eff} increased with time (Fig. 2). The minimum and near-equilibrium values of μ_{eff} are reported in Fig. 3 for experiments 1 and 2, and Table II for experiment 3, along with statistical differences. In both surface removal experiments (Fig. 3), no significant change was observed in μ_{\min} between the first and second test, either in the control group or in the treated group. For μ_{eq} , no statistical difference was observed between the first and second test in the control group (where the surface remained intact), or between the control and treated group in the first test (intact surfaces). However, a significant decrease was noted between the first and second test in the treated group (before and after surface removal, $P < 0.001$), and between the control and treated group in the second test (intact vs removed surface, $P < 0.001$). A statistical increase was found in μ_{\min} between experiment 1 and experiment 2 ($P < 0.05$), indicating increasing friction coefficient with normal force. However, no statistical difference was found in μ_{eq} between the two experiments. No statistical difference was observed in the creep

response before and after surface removal, as shown for example in the specimens of experiment 2 (Fig. 4).

In experiment 3, μ_{\min} was significantly smaller ($P < 0.01$) and μ_{eq} was significantly higher ($P < 0.001$) at the articular surface than on the microtomed deep zone.

Immunohistochemical staining showed SZP present in groups I and II, at the intact articular surface and within the top 20 μm from the surface (Fig. 5). In group III, SZP was absent at the microtomed surface. No staining was found in the deep zone in any of the three groups.

The average surface roughness was $R_a = 379 \pm 83$ nm for samples with intact articular surface (group 1), $R_a = 615 \pm 143$ nm for samples with a microtomed superficial zone (group 2), and $R_a = 795 \pm 208$ nm at the microtomed deep zone (group 3). Significant differences were found in the surface roughness between groups 1 and 2 ($P < 0.001$) and between groups 1 and 3 ($P < 0.001$). The surface topography of microtomed surfaces was also found to be quite different from intact cartilage (Fig. 6). The articular surface of intact specimens was largely fibrillar, showing scattered protuberances likely representing sub-surface chondrocytes. Microtomed surfaces revealed no distinct collagen network, though distinct pits were apparent which might have resulted from chondrocytes sheared away during surface removal. Parallel grooves were also observed, likely produced by the microtome blade.

Discussion

The objective of the current study was to test the hypothesis that the topmost superficial zone of articular

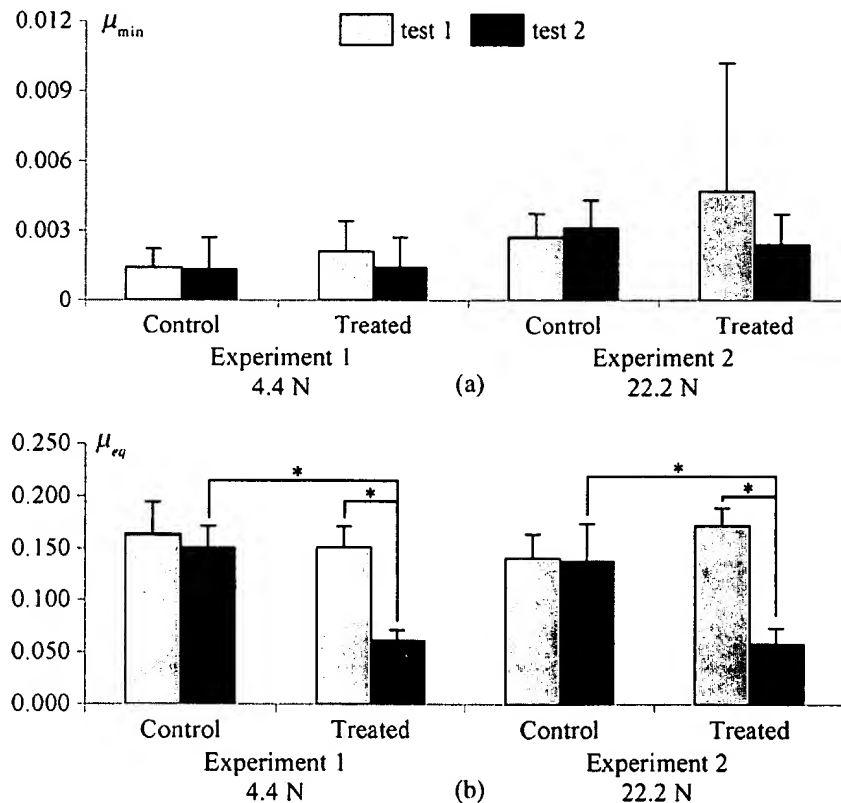


Fig. 3. Summary of frictional results from surface removal tests. Microtomed specimens are in test 2 of the treated group. (a) μ_{\min} ; (b) μ_{eq} ; * $P \leq 0.001$.

Table II

Summary of frictional results from articular surface vs deep zone. Last column shows P value of surface vs deep zone. P -value for surface vs deep appears in the first row for μ_{\min} and second row for μ_{eq}

Experiment 3 (22.2 N)						P value
Surface			Deep			
<i>h</i> (mm)	μ_{\min}	μ_{eq}	<i>h</i> (mm)	μ_{\min}	μ_{eq}	
1.96 ± 0.24	0.003 ± 0.0012	0.152 ± 0.013	1.96 ± 0.24	0.023 ± 0.021	0.060 ± 0.023	<0.01
						<0.001

cartilage, where SZP is localized¹³, has special frictional properties. This was investigated by performing *in-vitro* frictional tests between articular cartilage and glass, before and after removal of the superficial tangential zone ($\sim 100 \mu\text{m}$ thick) in cylindrical cartilage plugs. Results confirm previous findings that the friction coefficient increases with time under a constant applied load (Fig. 2)^{10,17,18}. This time-dependent response of the friction coefficient has been shown to be inversely correlated with the time-dependent pressurization of the interstitial water of cartilage^{9,19} according to the formula

$$\mu_{\text{eff}} = \mu_{\text{eq}} [1 - (1 - \phi) W^P / W] \quad (1)$$

where W^P/W is the time-varying interstitial fluid load support and $1 - \phi$ is related to the porosity of the articular surfaces. When load is first applied onto cartilage, the maximum value of W^P/W is normally very high ($> 90\%$), producing a low friction coefficient $\mu_{\text{eff}} = \mu_{\min}$. Over time, if the interstitial fluid pressure subsides ($W^P/W = 0$), the friction coefficient achieves its highest value, $\mu_{\text{eff}} = \mu_{\text{eq}}$. Under physiological loading conditions it is believed that the interstitial fluid pressurization of cartilage always remains elevated^{9,19-21}, so that μ_{\min} is more representative of the values of the friction coefficient *in vivo*. This is supported by findings that prolonged frictional loading of cartilage under near-equilibrium conditions produces measurable wear²².

The current study shows that removal of the superficial tangential zone produces no significant change in the minimum friction coefficient, μ_{\min} , which is achieved immediately after loading (Fig. 3). In a counter-intuitive

finding, results also indicate that the long-term (near-equilibrium) friction coefficient, μ_{eq} , decreases after removal of the superficial tangential zone. Based on the inclusion of control groups in the experimental design, it can be concluded that observed differences arise exclusively from the removal of the superficial zone, since neither repeated testing of intact samples nor short-term freezing of samples on the microtome stage alter the frictional response. Coupled with the histological confirmation that SZP was present in intact specimens and absent in microtomed specimens, and the consistency between the results of experiment 1 (4.4 N normal load) and experiment 2 (22.2 N normal load), these results do not support the hypothesis that the topmost superficial zone of cartilage, where SZP is localized, has special properties which reduce the friction coefficient at the articular surface. It should be noted, however, that this study does not address whether SZP can help reduce wear at the articular surfaces. Similarly, it does not address the potential interaction between SZP and synovial fluid, since friction measurements were performed in saline.

To further investigate the counter-intuitive decrease in μ_{eq} after removal of the superficial tangential zone, surface roughness measurements were used to assess whether microtoming might have produced a smoother surface than in the intact specimen. However, AFM measurements demonstrated that surface roughness increased after microtoming, thus discounting this possibility. For intact specimens, AFM roughness measurements were comparable to measurements made on newborn calf cartilage using more traditional methods²³.

Since μ_{eq} was found to be lower just below the articular surface, the next logical step was to explore whether it might decrease further toward the deep zone. Results from experiment 3 (Table II) confirmed that this is indeed the case, showing a 60% reduction from 0.15 at the articular surface to 0.06 at the deep zone. Whether this decrease is monotonic across the entire depth of the articular layer would need to be confirmed from additional experiments. Interestingly, however, the minimum friction coefficient, which represents the more functional measure of friction under physiological loading conditions, increased from 0.003 at the intact articular surface to 0.023 at the microtomed deep zone. This finding is consistent with our expectation that the inhomogeneity of the cartilage ultrastructural organization, biochemical composition, and biomechanical properties through the depth is related to its function as a bearing material²⁴, and our earlier observation that the peak interstitial fluid load support is significantly lower in the deep zone ($W^P/W = 71 \pm 8\%$) than in the surface zone ($W^P/W = 94 \pm 4\%$)²⁵.

No specific mechanism is proposed at this time to explain the reduction in μ_{eq} with depth from the articular surface; any proposed mechanism would need to be consistent with our previous studies where it was observed that the

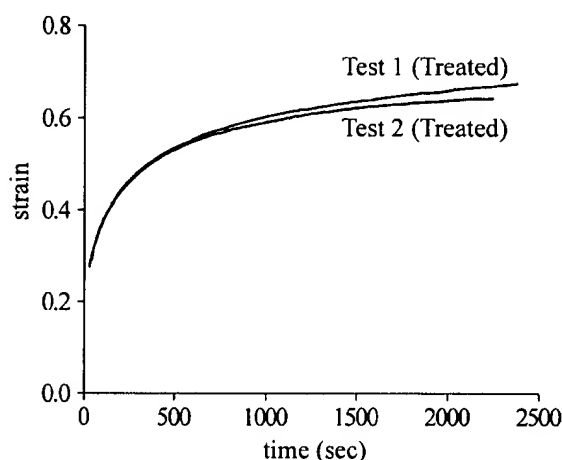


Fig. 4. Average compressive strain response (creep displacement/original thickness) over all specimens in experiment 2, for test 1 and test 2 of the treated group (before and after surface removal). The creep strain was 0.645 ± 0.082 in test 1 and 0.653 ± 0.157 in test 2, with no statistical difference observed ($P = 0.91$).

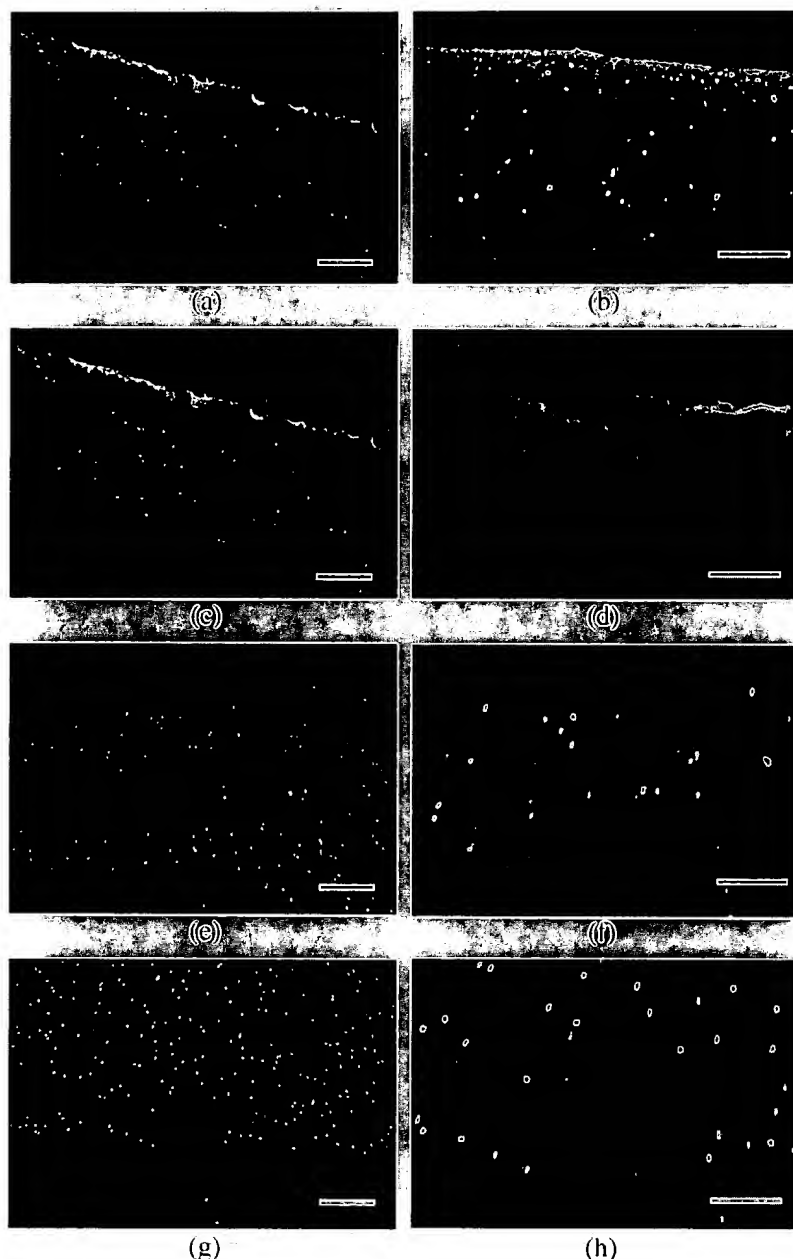


Fig. 5. Immunohistochemistry: Fluorescent images of representative samples from (a, b) group I and (c, d) group II, showed SZP present at the articular surface and within the superficial zone; (e, f) group III (microtomed surface) and (g, h) group III (microtomed deep zone) showed negligible SZP at the microtomed surface or the deep zone. (a, c, e, g) 20 \times magnification, scale bar = 100 μ m; (b, d, f, h) 50 \times magnification, scale bar = 50 μ m. Arrow indicates surface of interest in each image.

equilibrium friction coefficient increases with decreasing ionic strength of the saline bath, and decreases with increasing compressive strain²⁶.

One potential weakness of this study is that it measures the frictional response of cartilage against glass, whereas it might be argued that SZP is an effective boundary lubricant only for cartilage-against-cartilage. While this might indeed be the case, it should be noted that the minimum friction coefficients observed for intact cartilage in the current study ($\mu_{\min} \sim 0.0013$ – 0.0047) remain in the very low range of coefficients reported in the literature for a variety of testing

configurations, including cartilage-against-cartilage in synovial fluid^{2,27,28}. Thus testing against glass does not appear to have an adverse effect on the frictional response of cartilage.

Another potential weakness is that microtoming of the surface zone does not simply remove SZP but also alters the structure of the articular surface. This can produce confounding effects that make it difficult to reach a definitive conclusion on the role of SZP in cartilage lubrication. However, we believe that alternative approaches, such as enzymatic degradation of SZP, may not be sufficiently

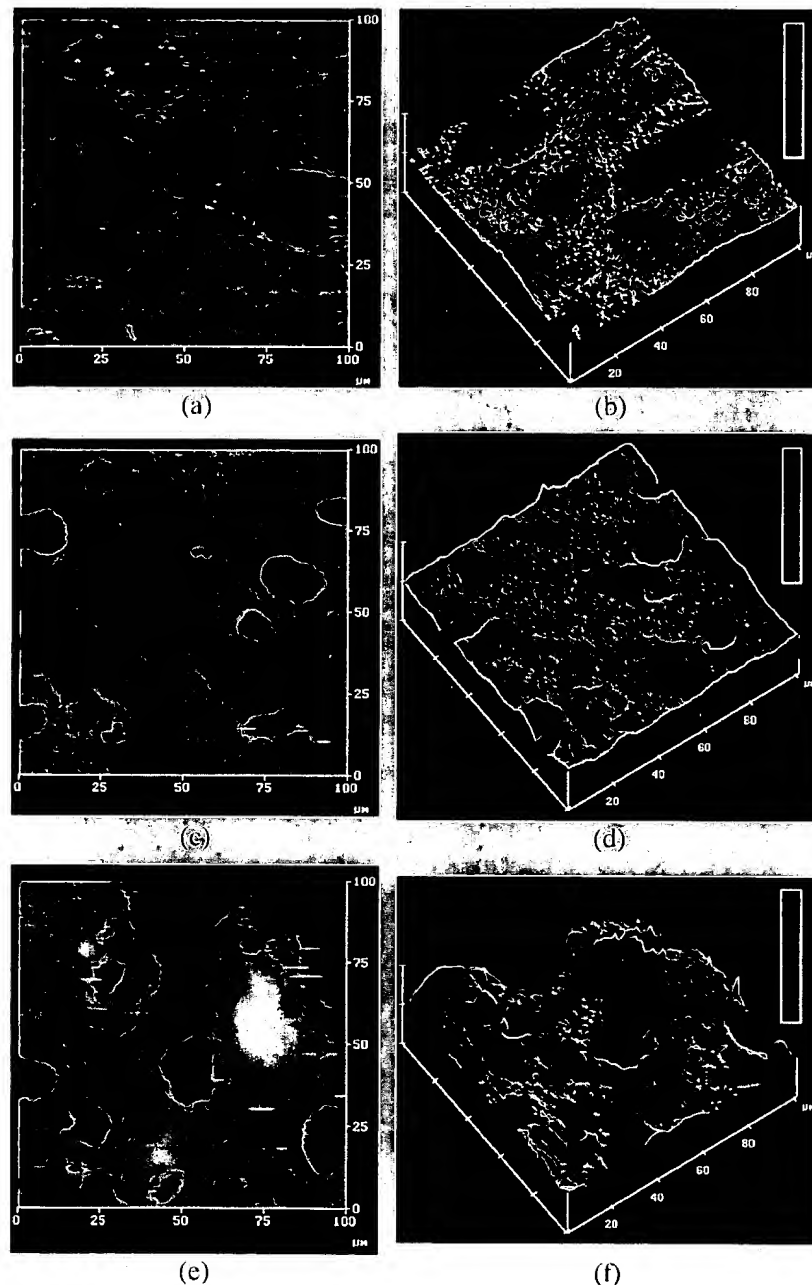


Fig. 6. Atomic force microscopy: (a, b) Intact articular surface from group 1; (c, d) microtomed surface zone from group 2; (e, f) microtomed deep zone from group 3. Z-direction scale bar = 5 μm .

selective and could produce other confounding effects, such as alterations in material properties and interstitial fluid load support, that may similarly complicate the interpretation of results. For example, in our recent study²⁹, it has been shown that proteoglycan degradation with chondroitinase ABC produces a statistically significant increase in μ_{min} and μ_{eq} , and a corresponding decrease in interstitial fluid load support. While enzymatic degradation studies may provide valuable insight, the current mechanical approach is equally necessary and useful in assessing the role of the superficial zone where SZP is localized. Importantly, neither the porosity³⁰ nor the mechanical

properties of bovine cartilage vary significantly in the topmost $\sim 100\text{--}200\text{ }\mu\text{m}$ region^{31,32}, as supported by our finding that the creep response remained virtually the same before and after surface removal (Fig. 4).

Despite the homology of SZP with lubricin^{11,12}, the current study does not discount the tribological properties of the lubricin present in synovial fluid^{4,5,33}. All measurements in this study were performed in PBS to reduce the potentially confounding effect of lubricin in synovial fluid. Other investigators have shown that testing the frictional response of articular cartilage in synovial fluid produces a moderately smaller friction coefficient than in Ringer's solution^{10,22},

which is likely due to the presence in synovial fluid of boundary lubricants such as lubricin, or phospholipids³⁴.

Acknowledgments

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